Abstract

The new SCALE™-2+ dual-driver core 2SC0435T combines unrivalled compactness with broad applicability. The driver was designed for universal applications requiring high reliability. The 2SC0435T drives all usual high-power IGBT modules up to 1700V. The embedded paralleling capability allows easy inverter design covering higher power ratings. Multi-level topologies are also supported.

The 2SC0435T is the most compact driver core in its power range available for industrial applications, with a footprint of only 57.2mm x 51.6mm and an insertion height of max. 20.5mm. It allows even the most restricted insertion spaces to be efficiently used.

Fig. 1   2SC0435T driver core
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Driver Overview

The 2SC0435T is a driver core equipped with Power Integrations' latest SCALE-2+ chipset /1/. The SCALE-2+ chipset is a set of application-specific integrated circuits (ASICs) that cover the main range of functions needed to design intelligent gate drivers. The SCALE-2+ driver chipset is a further development of the proven SCALE technology /2/.

The 2SC0435T targets medium-power, dual-channel IGBT and MOSFET applications. The driver supports switching up to 100kHz at best-in-class efficiency. The 2SC0435T comprises a complete dual-channel IGBT driver core, fully equipped with an isolated DC/DC converter, short-circuit protection, Advanced Active Clamping (AAC) and supply-voltage monitoring.

Fig. 2   Block diagram of the driver core 2SC0435T
Mechanical Dimensions

Fig. 3  Interactive 3D drawing of 2SC0435T2H0-17
Fig. 4   Mechanical drawing of 2SC0435T

The primary side and secondary side pin grid is 2.54mm (100mil) with a pin cross section of 0.64mm x 0.64mm. Total outline dimensions of the board are 57.2mm x 51.6mm. The total height of the driver is max. 20.5mm measured from the bottom of the pin bodies to the top of the populated PCB.

Recommended diameter of solder pads: Ø 2mm (79 mil)
Recommended diameter of drill holes: Ø 1mm (39 mil)
## Pin Designation

<table>
<thead>
<tr>
<th>Pin No. and Name</th>
<th>Function</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Primary Side</strong></td>
<td></td>
</tr>
<tr>
<td>1 VDC</td>
<td>DC/DC converter supply</td>
</tr>
<tr>
<td>2 SO1</td>
<td>Status output channel 1; normally high-impedance, pulled down to low on fault</td>
</tr>
<tr>
<td>3 SO2</td>
<td>Status output channel 2; normally high-impedance, pulled down to low on fault</td>
</tr>
<tr>
<td>4 MOD</td>
<td>Mode selection (direct/half-bridge mode)</td>
</tr>
<tr>
<td>5 TB</td>
<td>Set blocking time</td>
</tr>
<tr>
<td>6 VCC</td>
<td>Supply voltage; 15V supply for primary side</td>
</tr>
<tr>
<td>7 GND</td>
<td>Ground</td>
</tr>
<tr>
<td>8 INA</td>
<td>Signal input A; non-inverting input relative to GND</td>
</tr>
<tr>
<td>9 INB</td>
<td>Signal input B; non-inverting input relative to GND</td>
</tr>
<tr>
<td>10 GND</td>
<td>Ground</td>
</tr>
<tr>
<td><strong>Secondary Sides</strong></td>
<td></td>
</tr>
<tr>
<td>11 ACL1</td>
<td>Active clamping feedback channel 1; leave open if not used</td>
</tr>
<tr>
<td>12 VCE1</td>
<td>$V_{CE}$ sense channel 1; connect to IGBT collector through resistor network</td>
</tr>
<tr>
<td>13 REF1</td>
<td>Set $V_{CE}$ detection threshold channel 1; resistor to VE1</td>
</tr>
<tr>
<td>14 COM1</td>
<td>Secondary side ground channel 1</td>
</tr>
<tr>
<td>15 VE1</td>
<td>Emitter channel 1; connect to (auxiliary) emitter of power switch</td>
</tr>
<tr>
<td>16 VISO1</td>
<td>DC/DC output channel 1</td>
</tr>
<tr>
<td>17 GH1</td>
<td>Gate high channel 1; pulls gate high through turn-on resistor</td>
</tr>
<tr>
<td>18 GL1</td>
<td>Gate low channel 1; pulls gate low through turn-off resistor</td>
</tr>
<tr>
<td>19 Free</td>
<td></td>
</tr>
<tr>
<td>20 Free</td>
<td></td>
</tr>
<tr>
<td>21 Free</td>
<td></td>
</tr>
<tr>
<td>22 ACL2</td>
<td>Active clamping feedback channel 2; leave open if not used</td>
</tr>
<tr>
<td>23 VCE2</td>
<td>$V_{CE}$ sense channel 2; connect to IGBT collector through resistor network</td>
</tr>
<tr>
<td>24 REF2</td>
<td>Set $V_{CE}$ detection threshold channel 2; resistor to VE2</td>
</tr>
<tr>
<td>25 COM2</td>
<td>Secondary side ground channel 2</td>
</tr>
<tr>
<td>26 VE2</td>
<td>Emitter channel 2; connect to (auxiliary) emitter of power switch</td>
</tr>
<tr>
<td>27 VISO2</td>
<td>DC/DC output channel 2</td>
</tr>
<tr>
<td>28 GH2</td>
<td>Gate high channel 2; pulls gate high through turn-on resistor</td>
</tr>
<tr>
<td>29 GL2</td>
<td>Gate low channel 2; pulls gate low through turn-off resistor</td>
</tr>
</tbody>
</table>

Note: Pins with the designation “Free” are not physically present.
Recommended Interface Circuitry for the Primary Side Connector

Fig. 5 Recommended user interface of 2SC0435T (primary side)

Both ground pins must be connected together with low parasitic inductance. A common ground plane or wide tracks are strongly recommended. The connecting distance between ground pins must be kept at a minimum.

Description of Primary Side Interface

General

The primary side interface of the driver 2SC0435T is very simple and easy to use.

The driver primary side is equipped with a 10-pin interface connector with the following terminals:

- 2 x power-supply terminals
- 2 x drive signal inputs
- 2 x status outputs (fault returns)
- 1 x mode selection input (half-bridge mode / direct mode)
- 1 x input to set the blocking time

All inputs and outputs are ESD-protected. Moreover, all digital inputs have Schmitt-trigger characteristics.

VCC terminal

The driver has one VCC terminal on the interface connector to supply the primary side electronics with 15V.
VDC terminal

The driver has one VDC terminal on the interface connector to supply the DC-DC converters for the secondary sides.

VDC should be supplied with 15V. It is recommended to connect the VCC and VDC terminals to a common 15V power supply. In this case the driver limits the inrush current at startup and no external current limitation of the voltage source for VDC is needed.

MOD (mode selection)

The MOD input allows the operating mode to be selected with a resistor connected to GND.

Direct mode

If the MOD input is connected to GND, direct mode is selected. In this mode, there is no interdependence between the two channels. Input INA directly influences channel 1 while INB influences channel 2. High level at an input (INA or INB) always results in turn-on of the corresponding IGBT. In a half-bridge topology, this mode should be selected only when the dead times are generated by the control circuitry so that each IGBT receives its own drive signal.

Caution: Synchronous or overlapping timing of both switches of a half-bridge basically shorts the DC-link.

Half-bridge mode

If the MOD input is connected to GND with a resistor $72k < R_m < 181k$, half-bridge mode is selected. In this mode, the inputs INA and INB have the following functions: INA is the drive signal input while INB acts as the enable input (Fig. 6). It is recommended to place a capacitor $C_m = 22nF$ in parallel to $R_m$ in order to reduce the deviation between the dead times at the rising and falling edges of INA respectively.

When input INB is low level, both channels are blocked. If it goes high, both channels are enabled and follow the signal on the input INA. At the transition of INA from low to high, channel 2 turns off immediately and channel 1 turns on after a dead time $T_d$.

![Fig. 6 Signals in half-bridge mode](image-url)
The value of the dead time $T_d$ is determined by the value of the resistor $R_m$ according to the following formula (typical value):

$$R_m[\Omega] = 31.5 \cdot T_d[\mu s] + 52.7$$

with $0.6 \mu s < T_d < 4.1 \mu s$ and $72k \Omega < R_m < 181k \Omega$

Note that the dead time may vary from sample to sample. A tolerance of approximately ±20% may be expected. If higher timing precisions are required, Power Integrations recommends using the direct mode and generating the dead time externally (refer to the Application Note AN-1101 /4/).

**INA, INB (channel drive inputs, e.g. PWM)**

INA and INB are basically drive inputs, but their function depends on the MOD input (see above). They safely recognize signals in the whole logic-level range between 3.3V and 15V. Both input terminals feature Schmitt-trigger characteristics (refer to the driver data sheet /3/). An input transition is triggered at any edge of an incoming signal at INA or INB.

**SO1, SO2 (status outputs)**

The outputs SOx have open-drain transistors. When no fault condition is detected, the outputs have high impedance. An internal current source of 500μA pulls the SOx outputs to a voltage of about 4V when left open. When a fault condition (primary side supply undervoltage, secondary side supply undervoltage, IGBT short-circuit or overcurrent) is detected, the corresponding status output SOx goes to low (connected to GND).

The diodes D₁ and D₂ must be Schottky diodes and must only be used when using 3.3V logic. For 5V…15V logic, they can be omitted.

The maximum SOx current in a fault condition must not exceed the value specified in the driver data sheet /3/.

Both SOx outputs can be connected together to provide a common fault signal (e.g. for one phase). However, it is recommended to evaluate the status signals individually to allow fast and precise fault diagnosis.

**How the status information is processed**

a) A fault on the secondary side (detection of short-circuit of IGBT module or supply undervoltage) is transmitted to the corresponding SOx output immediately. The SOx output is automatically reset (returning to a high impedance state) after a blocking time $T_b$ has elapsed (refer to “TB (input for adjusting the blocking time $T_b$)” for timing information).

b) A supply undervoltage on the primary side is indicated to both SOx outputs at the same time. Both SOx outputs are automatically reset (returning to a high impedance state) when the undervoltage on the primary side disappears.

**TB (input for adjusting the blocking time $T_b$)**

The terminal TB allows the blocking time to be set by connecting a resistor $R_b$ to GND (Fig. 5). The following equation calculates the value of $R_b$ connected between pins TB and GND in order to program the desired blocking time $T_b$ (typical value):

$$R_b[\Omega] = 1.0 \cdot T_b[ms] + 51$$

with $20ms < T_b < 130ms$ and $71k \Omega < R_b < 181k \Omega$

The blocking time can also be set to a minimum of 9μs (typical) by selecting $R_b=0\Omega$. The terminal TB must not be left floating.
Note: It is also possible to apply a stabilized voltage at TB. The following equation is used to calculate the voltage $V_b$ between TB and GND in order to program the desired blocking time $T_b$ (typical value):

$$V_b[V] = 0.02 \cdot T_b[ms] + 1.02 \quad \text{with} \quad 20\text{ms}<T_b<130\text{ms} \text{ and } 1.42<V_b<3.62\text{V}$$

**Recommended Interface Circuitry for the Secondary Side Connectors**

![Recommended Interface Circuitry](image)

**Fig. 7** Recommended user interface of 2SC0435T with Advanced Active Clamping (secondary sides)

**Description of Secondary Side Interfaces**

**General**

Each driver’s secondary side (driver channel) is equipped with an 8-pin interface connector with the following terminals (x stands for the number of the drive channel 1 or 2):

- 1 x DC/DC output terminal VISOx
- 1 x emitter terminal VEx
- 1 x reference terminal REFx for overcurrent or short-circuit protection
- 1x collector sense terminal VCEx
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- 1x active clamping terminal ACLx
- 1x turn-on gate terminals GHx
- 1x turn-off gate terminals GLx

All inputs and outputs are ESD-protected.

DC/DC output (VISOx), emitter (VEx) and COMx terminals

The driver is equipped with blocking capacitors on the secondary side of the DC/DC converter (for values, refer to the data sheet /3/).

Power semiconductors with a gate charge of up to 3µC can be driven without additional capacitors on the secondary side. For IGBTs or MOSFETs with a higher gate charge, a minimum value of 3µF external blocking capacitance is recommended for every 1µC gate charge beyond 3µC. The blocking capacitors must be placed between VISOx and VEx (C_{1x} in Fig. 7) as well as between VEx and COMx (C_{2x} in Fig. 7). They must be connected as close as possible to the driver’s terminal pins with minimum inductance. It is recommended to use the same capacitance value for both C_{1x} and C_{2x}. Ceramic capacitors with a dielectric strength >20V are recommended.

If the capacitances C_{1x} or C_{2x} exceed 150µF, please contact Power Integrations' support service.

No static load must be applied between VISOx and VEx, or between VEx and COMx. A static load can be applied between VISOx and COMx if necessary.

Reference terminal (REFx)

The reference terminal REFx allows the threshold to be set for short-circuit and/or overcurrent protection with a resistor placed between REFx and VEx. A constant current of 150µA is provided at pin REFx.

Collector sense (VCEx)

The collector sense must be connected to the IGBT collector or MOSFET drain with the circuit shown in Fig. 7 in order to detect an IGBT or MOSFET overcurrent or short-circuit.

- It is recommended to dimension the resistor value of R_{vce} in order to get a current of about 0.6-1mA flowing through R_{vce} (e.g. 1.2-1.8MΩ for V_{DC-LINK}=1200V). The current through R_{vce} must not exceed 1mA. It is possible to use a high-voltage resistor as well as series connected resistor. In any case, the min. creepage distance related to the application must be considered.
- The diode D_{6x} must have a very low leakage current and a blocking voltage of >40V (e.g. BAS416). Schottky diodes must be explicitly avoided.

For more details about the functionality of this feature and the dimensioning of the response time, refer to “VCE monitoring / short-circuit protection” on page 15.

Active clamping (ACLx)

Active clamping is a technique designed to partially turn on the power semiconductor as soon as the collector-emitter (drain-source) voltage exceeds a predefined threshold. The power semiconductor is then kept in linear operation.

Basic active clamping topologies implement a single feedback path from the IGBT’s collector through transient voltage suppressor devices (TVS) to the IGBT gate. The 2SC0435T supports Power Integrations’ Advanced
Active Clamping, where the feedback is also provided to the driver’s secondary side at pin ACLx: as soon as the voltage on the right side of the $20\Omega$ resistor (Fig. 7) exceeds about 1.3V, the turn-off MOSFET is progressively switched off in order to improve the effectiveness of the active clamping and to reduce the losses in the TVS. The turn-off MOSFET is completely off when the voltage on the right side of the $20\Omega$ resistors (Fig. 7) approaches 20V (measured to COMx).

It is recommended to use the circuit shown in Fig. 7. The following parameters must be adapted to the application:

- **TVS D$_{1x}$, D$_{2x}$**: It is recommended to use:
  - Six 80V TVS with 600V IGBTs with DC-link voltages up to 430V. Good clamping results can be obtained with five unidirectional TVS P6SMBJ70A and one bidirectional TVS P6SMBJ70CA from Semikron or with five unidirectional TVS SMBJ70A-E3 and one bidirectional TVS SMBJ70CA-E3 from Vishay.
  - Six 150V TVS with 1200V IGBTs with DC-link voltages up to 800V. Good clamping results can be obtained with five unidirectional TVS SMBJ130A-E3 and one bidirectional TVS SMBJ130CA-E3 from Vishay or five unidirectional TVS SMBJ130A-TR from ST and one bidirectional TVS P6SMBJ130CA from Diotec.
  - Six 220V TVS with 1700V IGBTs with DC-link voltages up to 1200V. Good clamping results can be obtained with five unidirectional TVS P6SMB220A and one bidirectional TVS P6SMB220CA from Diotec or five unidirectional TVS SMBJ188A-E3 and one bidirectional TVS SMBJ188CA-E3 from Vishay.

At least one bidirectional TVS (D$_{2x}$) per channel must be used in order to avoid negative current flowing through the TVS chain during turn-on of the antiparallel diode of the IGBT module due to its forward recovery behavior. Such a current could, depending on the application, lead to undervoltage of the driver secondary voltage VISOx to VEEx (15V).

Note that it is possible to modify the number of TVS in a chain. The active clamping efficiency can be improved by increasing the number of TVS used in a chain if the total threshold voltage remains at the same value. Note also that the active clamping efficiency is highly dependent on the type of TVS used (e.g. manufacturer).

- **R$_{aclx}$ and C$_{aclx}$**: These parameters allow the effectiveness of the active clamping as well as the losses in the TVS and the IGBT to be optimized. It is recommended to determine the value with measurements in the application. Typical values are: $R_{aclx}=0...150\Omega$ and $R_{aclx}*C_{aclx}=100\text{ns}...500\text{ns}$. $R_{aclx}=0\Omega$ is recommended to improve the effectiveness of active clamping.

- **D$_{3x}$, D$_{4x}$ and D$_{5x}$**: It is recommended to use Schottky diodes with blocking voltages $>35V$ ($>1A$ depending on the application).

Please note that the $20\Omega$ resistor as well as diodes D$_{3x}$, D$_{4x}$ and D$_{5x}$ must not be omitted if AAC is used. If AAC is not used, the $20\Omega$ resistor as well as diodes D$_{3x}$ and D$_{4x}$ can be omitted.

**Application note AN-1302 /7/** gives information about Dynamic Advanced Active Clamping (DA$^2$C) which allows increasing the DC-link voltage to higher values in non-switching off-state condition.

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**Gate turn-on (GHx) and turn-off (GLx) terminals**

These terminals allow the turn-on (GHx) and turn-off (GLx) gate resistors to be connected to the gate of the power semiconductor. The GHx and GLx pins are available as separated terminals in order to set the turn-on and turn-off resistors independently without the use of an additional diode. Please refer to the driver data sheet /3/ for the limit values of the gate resistors used.
A resistor between GLx and COMx of 4.7kΩ (other values are also possible) may be used in order to provide a low-impedance path from the IGBT/MOSFET gate to the emitter/source even if the driver is not supplied with power. No static load (e.g. resistors) must be placed between GLx and the emitter terminal VEx.

Note however that it is not advisable to operate the power semiconductors within a half-bridge with a driver in the event of a low supply voltage. Otherwise, a high rate of increase of $V_{CE}$ may cause partial turn-on of these IGBTs.

### How Do 2SC0435T SCALE-2+ Drivers Work in Detail?

#### Power supply and electrical isolation

The driver is equipped with a DC/DC converter to provide an electrically insulated power supply to the gate driver circuitry. All transformers (DC/DC and signal transformers) feature safe isolation to EN 50178, protection class II between primary side and either secondary side.

Note that the driver requires a stabilized supply voltage.

#### Power-supply monitoring

The driver’s primary side as well as both secondary-side driver channels are equipped with a local undervoltage monitoring circuit.

In the event of a primary-side supply undervoltage, the power semiconductors are driven with a negative gate voltage to keep them in the off-state (the driver is blocked) and the fault is transmitted to both outputs SO1 and SO2 until the fault disappears.

In case of a secondary-side supply undervoltage, the corresponding power semiconductor is driven with a negative gate voltage to keep it in the off-state (the channel is blocked) and a fault condition is transmitted to the corresponding SOx output. The SOx output is automatically reset (returning to a high impedance state) after the blocking time.
Each channel of the 2SC0435T driver is equipped with a $V_{CE}$ monitoring circuit. The recommended external circuitry is shown in Fig. 7. A resistor ($R_{thx}$ in Fig. 7) is used as the reference element for defining the turn-off threshold. The value of the current through $R_{thx}$ is 150μA (typical). It is recommended to choose threshold levels of about 10V ($R_{thx}$ values around 68kΩ). In this case the driver will safely protect the IGBT against short-circuit, but not necessarily against overcurrent. Overcurrent protection has a lower timing priority and is recommended to be realized within the host controller.

In order to ensure that the 2SC0435T can be applied as universally as possible, the response time capacitor $C_{ax}$ is not integrated in the driver, but must be connected externally.

During the response time, the $V_{CE}$ monitoring circuit is inactive. The response time is the time that elapses after turn-on of the power semiconductor until the collector/drain voltage is measured (Fig. 8).

Both IGBT collector-emitter voltages are measured individually. $V_{CE}$ is checked after the response time at turn-on to detect a short circuit or overcurrent. If the measured $V_{CE}$ at the end of the response time is higher than the programmed threshold $V_{thx}$, the driver detects a short circuit or overcurrent. The driver then switches off the corresponding power semiconductor. The fault status is immediately transferred to the corresponding SOx output of the affected channel. The power semiconductor is kept in off-state (non-conducting) and the fault is shown at pin SOx as long as the blocking time $T_b$ is active.

The blocking time $T_b$ is applied independently to each channel. $T_b$ starts as soon as $V_{CE}$ exceeds the threshold of the $V_{CE}$ monitoring circuit outside the response time span.

The value of the response time capacitors $C_{ax}$ can be determined with the following table in order to set the desired response time ($R_{vcex}=1.8MΩ$, DC-link voltage $V_{DC-LINK}>550V$):

<table>
<thead>
<tr>
<th>$C_{ax}$ [pF]</th>
<th>$R_{thx}$ [kΩ]</th>
<th>$V_{thx}$ [V]</th>
<th>Response time [μs]</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>43 / 6.45</td>
<td></td>
<td>1.2</td>
</tr>
<tr>
<td>15</td>
<td>43 / 6.45</td>
<td></td>
<td>3.2</td>
</tr>
<tr>
<td>22</td>
<td>43 / 6.45</td>
<td></td>
<td>4.2</td>
</tr>
<tr>
<td>33</td>
<td>43 / 6.45</td>
<td></td>
<td>5.8</td>
</tr>
<tr>
<td>47</td>
<td>43 / 6.45</td>
<td></td>
<td>7.8</td>
</tr>
<tr>
<td>0</td>
<td>68 / 10.2</td>
<td></td>
<td>1.5</td>
</tr>
<tr>
<td>15</td>
<td>68 / 10.2</td>
<td></td>
<td>4.9</td>
</tr>
<tr>
<td>22</td>
<td>68 / 10.2</td>
<td></td>
<td>6.5</td>
</tr>
<tr>
<td>33</td>
<td>68 / 10.2</td>
<td></td>
<td>8.9</td>
</tr>
<tr>
<td>47</td>
<td>68 / 10.2</td>
<td></td>
<td>12.2</td>
</tr>
</tbody>
</table>

Table 1  Typical response time in function of the capacitance $C_{ax}$ and the resistance $R_{thx}$
As the parasitic capacitances on the host PCB may influence the response time it is recommended to measure it in the final design. It is important to define a response time which is smaller than the max. allowed short-circuit duration of the used power semiconductor.

Note that the response time increases at DC-link voltage values lower than 550V and/or higher threshold voltage values $V_{\text{thx}}$. The response time will decrease at lower threshold voltage values.

**Desaturation protection with sense diodes**

If desaturation protection with sense diodes is required with 2SC0435T, please refer to the application note AN-1101 /4/.

**Parallel connection of 2SC0435T**

If parallel connection of 2SC0435T drivers is required, please refer to the application note AN-0904 /5/.

**3-level or multilevel topologies**

If 2SC0435T drivers are to be used in 3-level or multilevel topologies, please refer to the application note AN-0901 /6/.

**Additional application support for 2SC0435T**

For additional application support using 2SC0435T drivers, please refer to the application note AN-1101 /4/.

### Electrical Ratings for UL recognized types

The following ratings apply for the UL recognized product versions according to the UL definitions:

<table>
<thead>
<tr>
<th>Power/Channel</th>
<th>Gate Current</th>
<th>Control Circuit (Input/Output)</th>
<th>System Voltage</th>
</tr>
</thead>
<tbody>
<tr>
<td>4W</td>
<td>35A</td>
<td>15Vdc</td>
<td>730Vac/dc</td>
</tr>
</tbody>
</table>
Bibliography

/1/ Paper: Smart Power Chip Tuning, Bodo’s Power Systems, May 2007
/2/ “Description and Application Manual for SCALE™ Drivers”, Power Integrations
/3/ Data sheet SCALE™-2+ driver core 2SC0435T, Power Integrations
/4/ Application note AN-1101: Application with SCALE™-2 and SCALE™-2+ Gate Driver Cores, Power Integrations
/5/ Application note AN-0904: Direct Paralleling of SCALE™-2 Gate Driver Cores, Power Integrations
/6/ Application note AN-0901: Methodology for Controlling Multi-Level Converter Topologies with SCALE™-2 IGBT Drivers, Power Integrations
/7/ Application note AN-1302: Dynamic Advanced Active Clamping (DA²C), Power Integrations

Note: The Application Notes are available on the Internet at www.power.com/igbt-driver/go/app-note and the papers at www.power.com/igbt-driver/go/papers.

The Information Source: SCALE-2 and SCALE-2+ Driver Data Sheets

Power Integrations offers the widest selection of gate drivers for power MOSFETs and IGBTs for almost any application requirements. The largest website on gate-drive circuitry anywhere contains all data sheets, application notes and manuals, technical information and support sections: www.power.com.

Quite Special: Customized SCALE-2 and SCALE-2+ Drivers

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<td>Dual-channel SCALE-2+ driver core (Lead free, connector pin length: 5.84mm, increased EMI capability)</td>
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Product home page: [www.power.com/igbt-driver/go/2SC0435T](http://www.power.com/igbt-driver/go/2SC0435T)

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## Preliminary Description & Application Manual

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